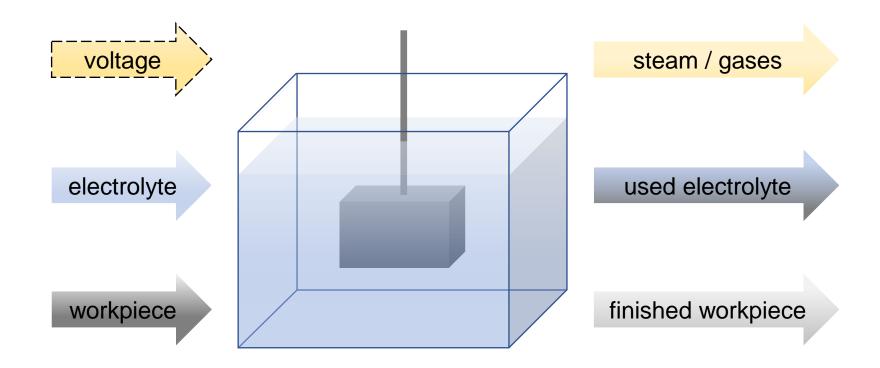


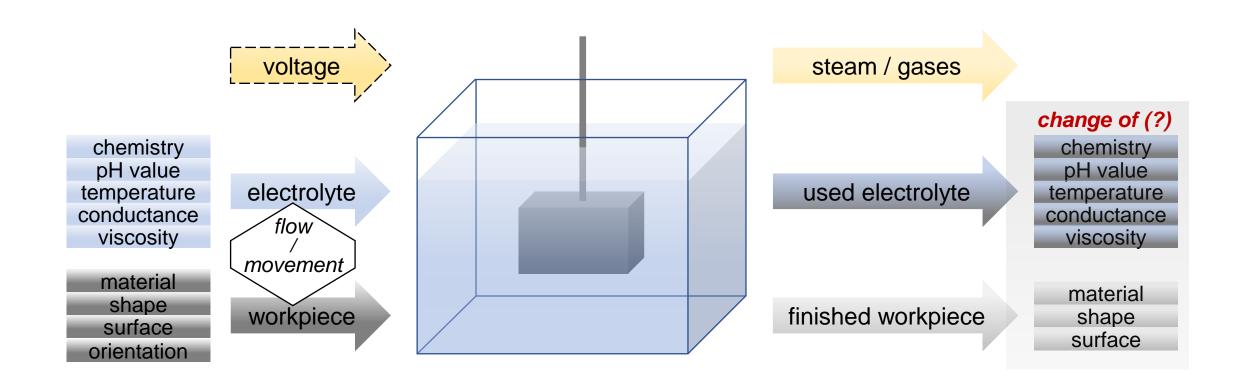


UNDERSTANDING PEP

Part 1: Mechanisms, Chemistry, Parameters

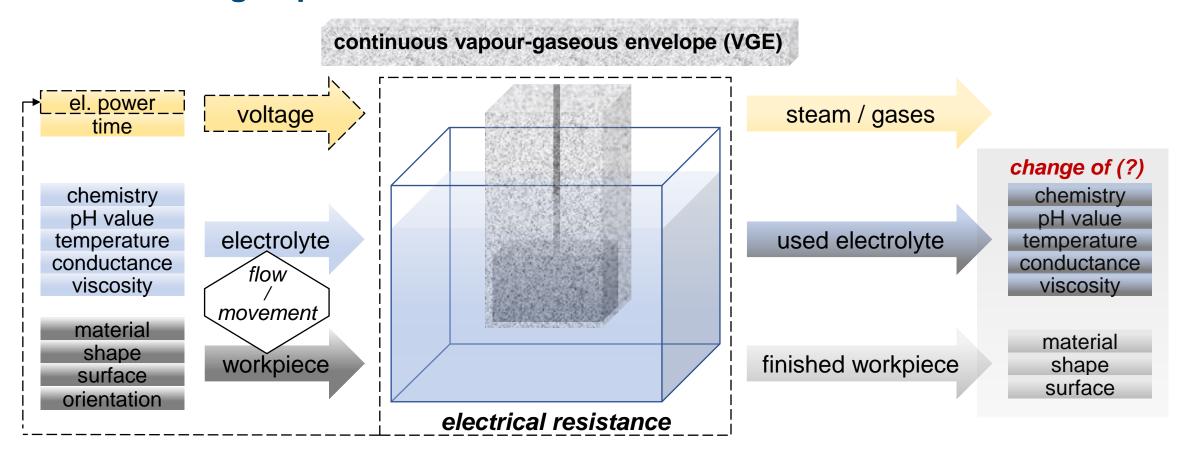






(not) a simple process with complex relations?!

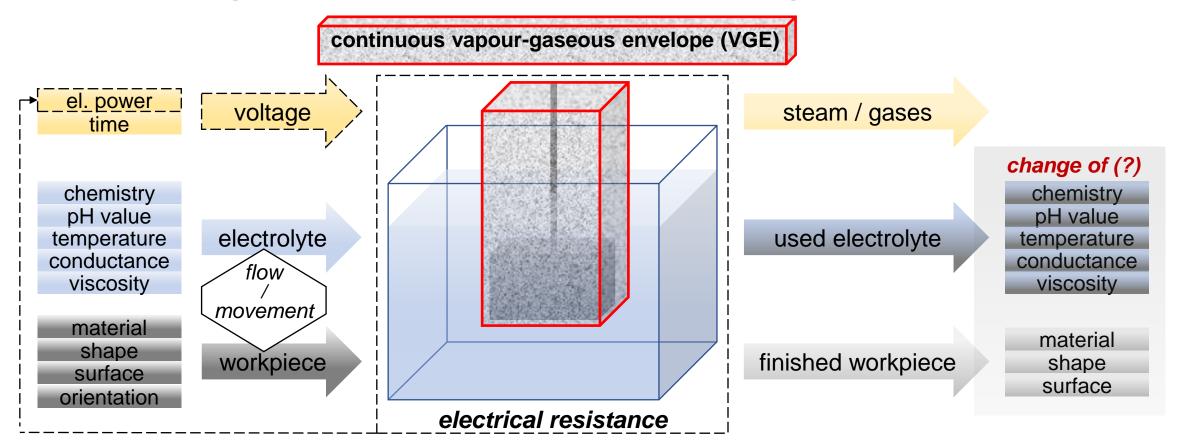




Special feature: Plasma forms under atmospheric pressure in liquid



vapour-gaseous envelope (VGE)

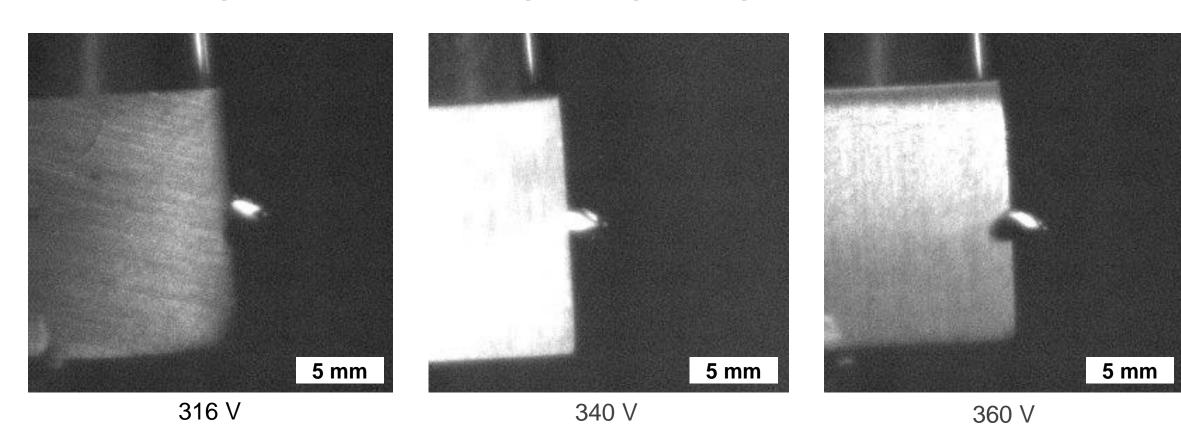


(not) a simple process with complex relations?!



Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms



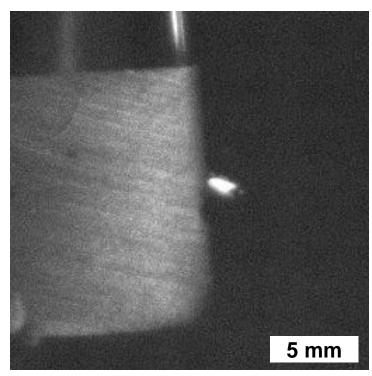
→ Very fast and high hydrodynamic process

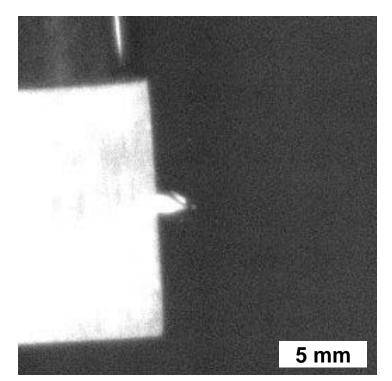


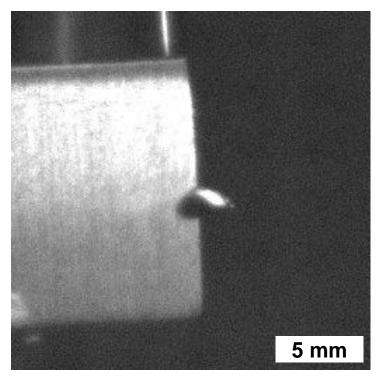
Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 0 ms







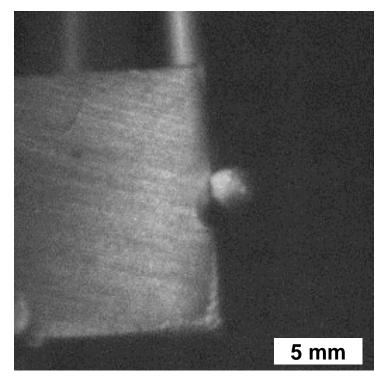
316 V 340 V 360 V

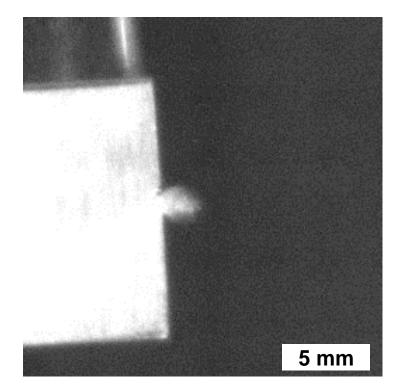


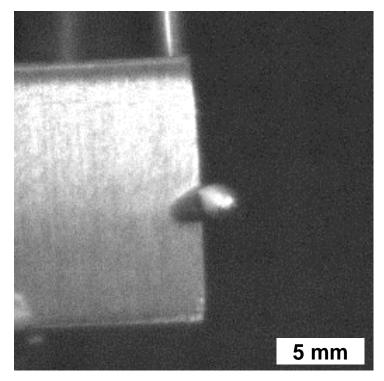
Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 0.33 ms







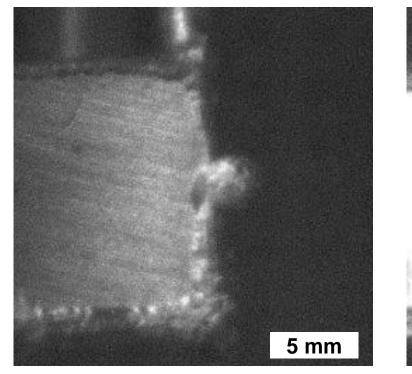
316 V 340 V 360 V

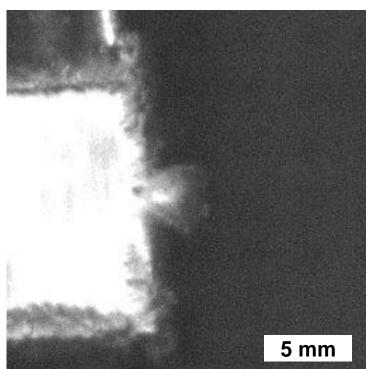


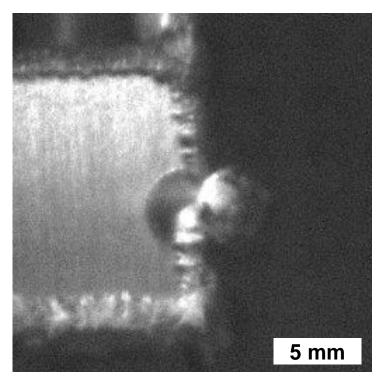
Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 1 ms







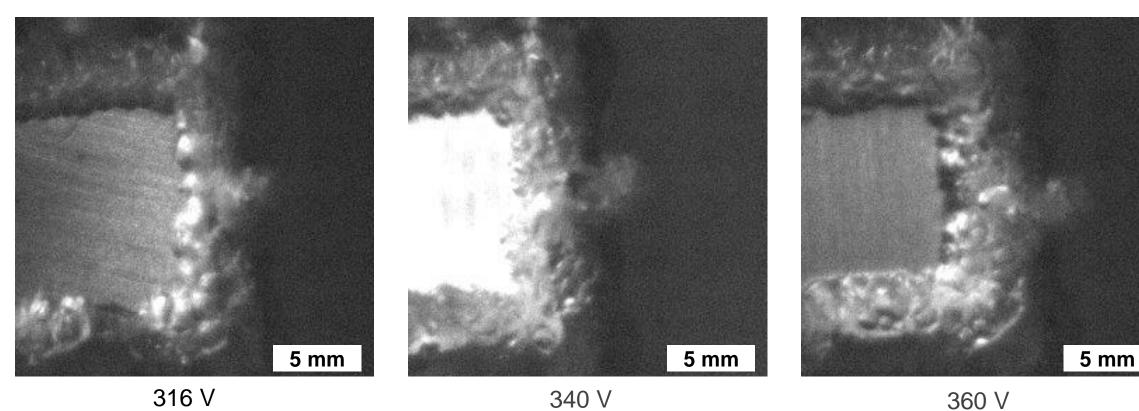
316 V 340 V 360 V



Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 2 ms



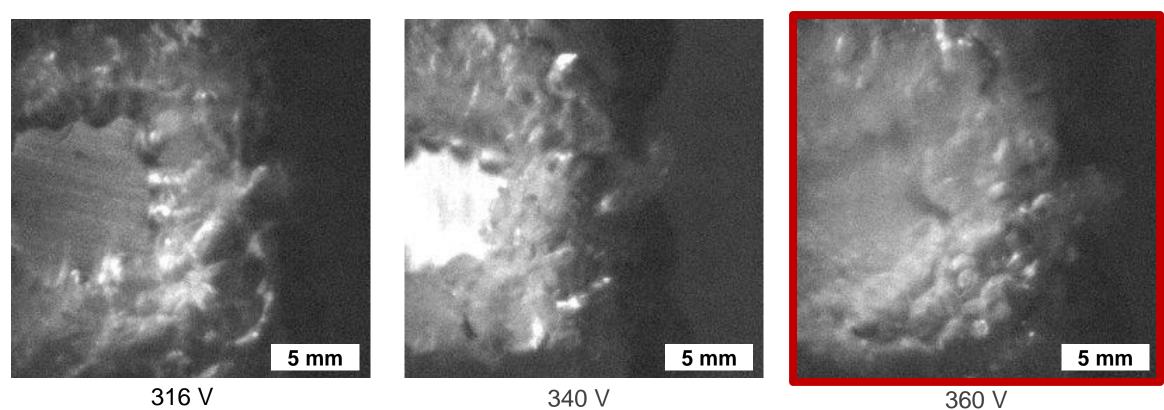
→ Very fast and high hydrodynamic process



Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 3.17 ms



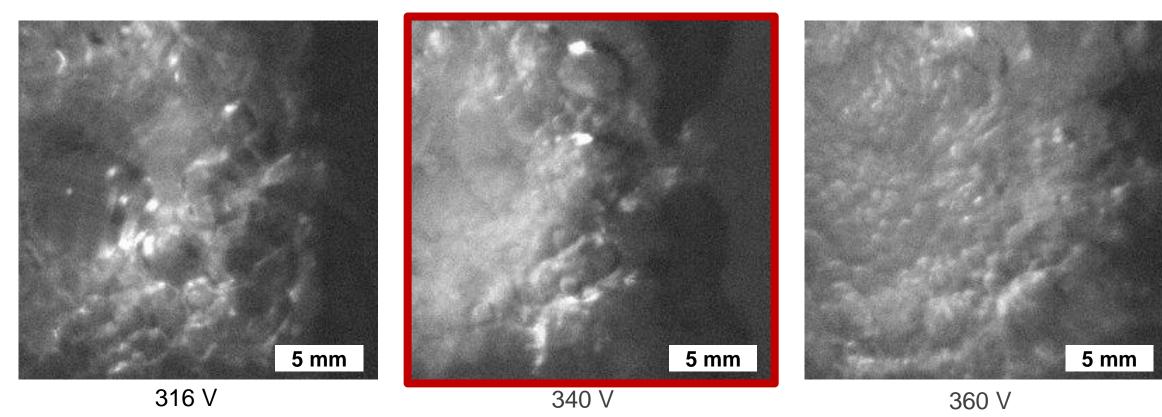
→ Very fast and high hydrodynamic process



Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 4.17 ms

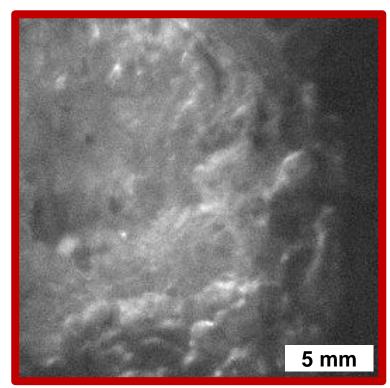


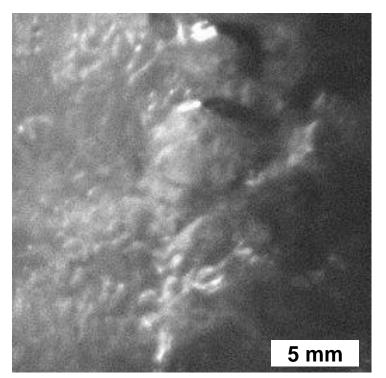


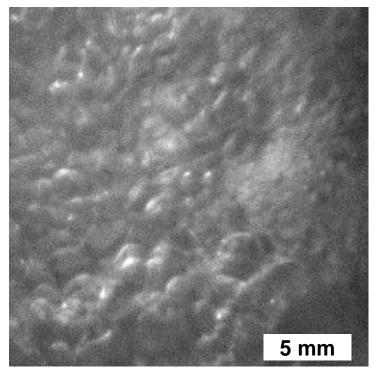
Developement of VGE

High-speed Camera recordings starting submerged: 0.0 ms ≤ t ≤ 8.33 ms

$$\rightarrow$$
 t = 5.00 ms

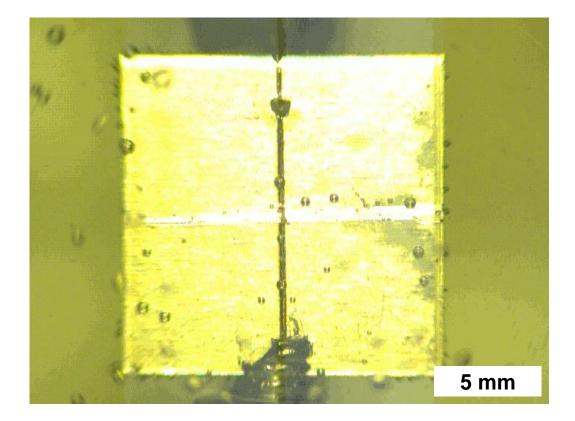






316 V 340 V 360 V

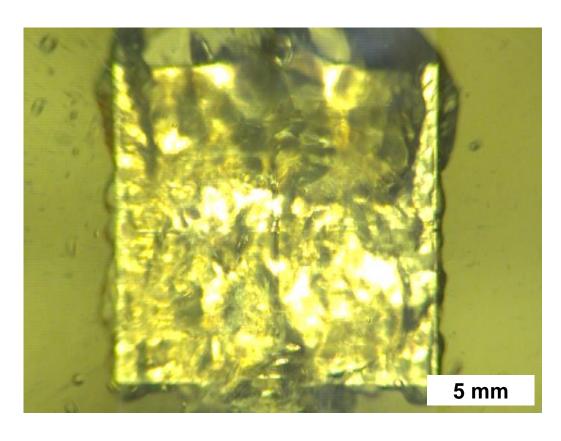




stable process and continuose VGE



stable process and continuose VGE



continuose: → allover (vs. lokal breakdowns)

→ development

+

growing/merging

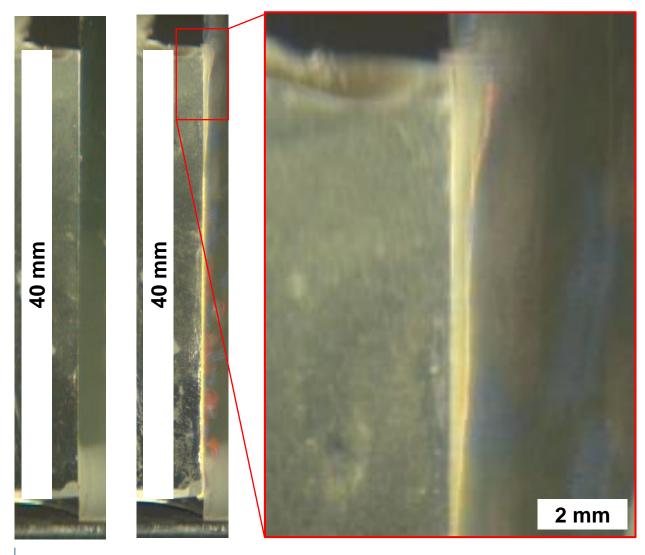
+

upraising and releasing from sample

... and

pulsating: → (lokal) thickness changes dynamically





VGE conditions over heigh

"cross section" of VGE / plasma region:

- → sum up of vape/gas from bottom to top
- → (average) thickness grows from bottom to top



non-uniform conditions:

- → stronger material remove rate (MRR) and
- → higher glossdown(side) than up(side)



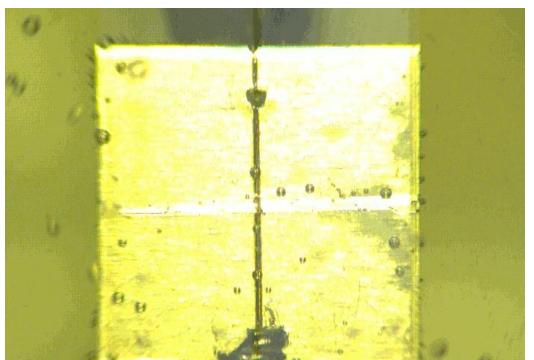
effect of electrolyt flow on VGE

continuous vapour-gaseous envelope (VGE) el. power voltage steam / gases time change of (?) chemistry chemistry pH value pH value electrolyte used electrolyte temperature temperature conductance conductance flow viscosity viscosity movement material material shape finished workpiece workpiece shape surface surface orientation electrical resistance

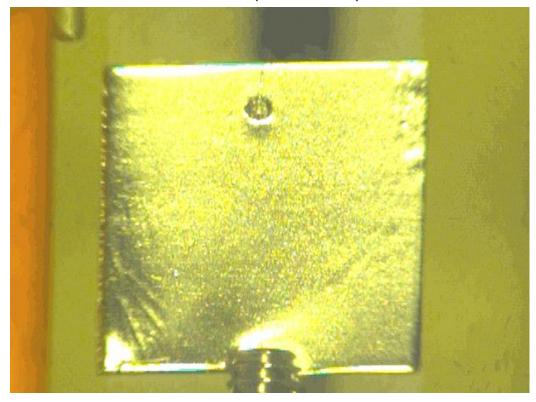


effect of electrolyt flow on VGE

no additional flow: 0 m/s



additional flow (from left): 1.2 m/s

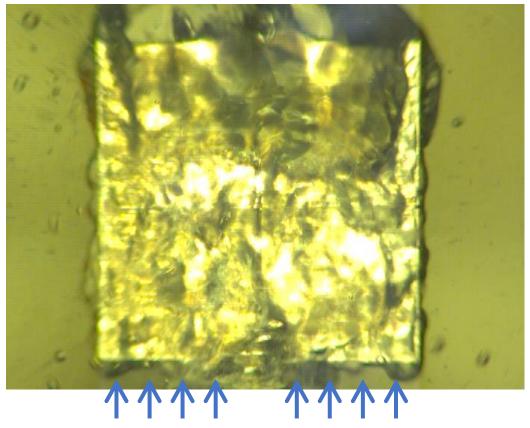




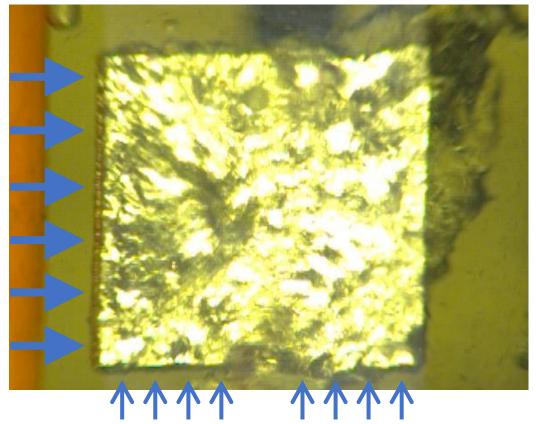
effect of electrolyt flow on VGE

no additional flow: 0 m/s

additional flow (from left): 1.2 m/s



"natural" electrolyte streaming



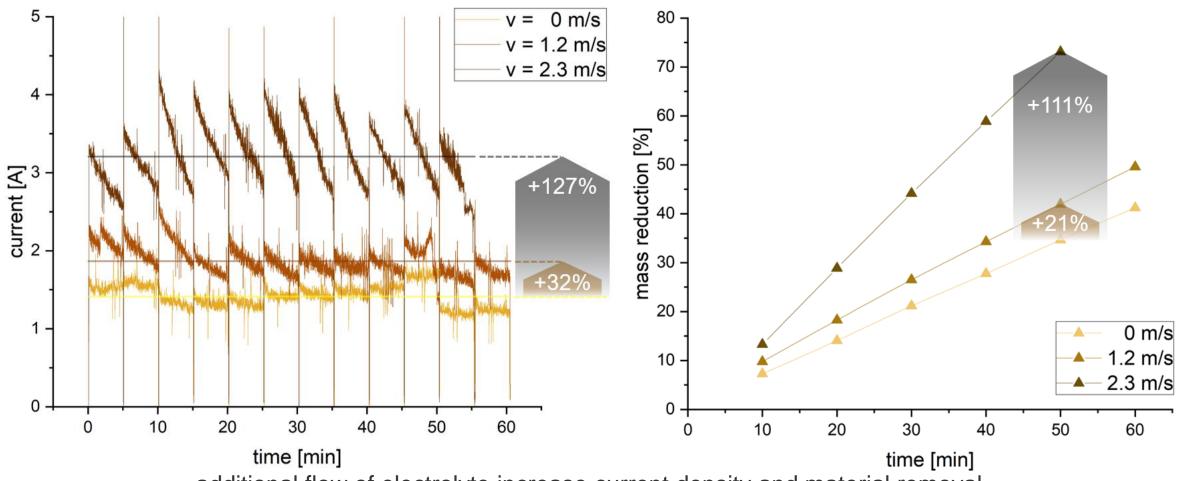


effect of electrolyt flow on VGE

2.3 m/s 0 m/s 1.2 m/s min 40 min



effect of electrolyt flow on VGE



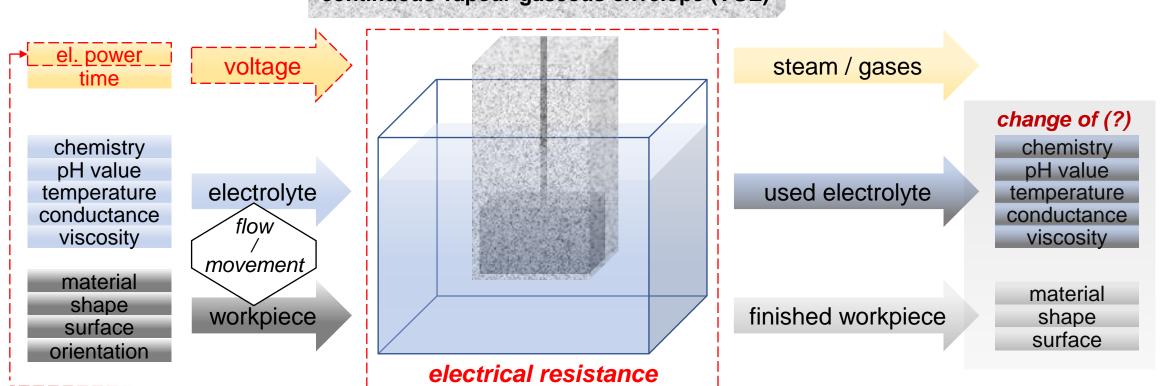
additional flow of electrolyte increase current density and material removal

→ Relative movement surface – electrolyte: very strong effect on PeP-results!



energy

continuous vapour-gaseous envelope (VGE)





energy

energy conservation law:

$$E_{input} = E_{output}$$

E(electrical + thermal + chemical) = E(electrical + thermal + chemical)

If the chemistry of the electrolyte has the opportunity to dissolve the workpiece material, a part of the input **electrical charge** will lead to the oxidation of the anodic workpiece (= material removal).

If not, it is mainly a **change of electric into thermal energy** (material removal and/or surface smoothening could be possible by local melting/evaporating of metal).

electrical charges (current I) = main drivers of PeP

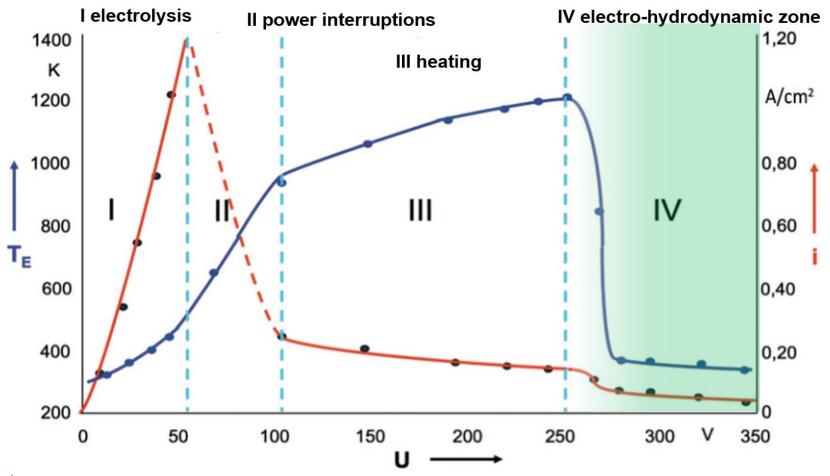
H

voltage range ($U = \sim 280$ to ~ 370 V) for material removal AND high surface finish



lower voltage limit

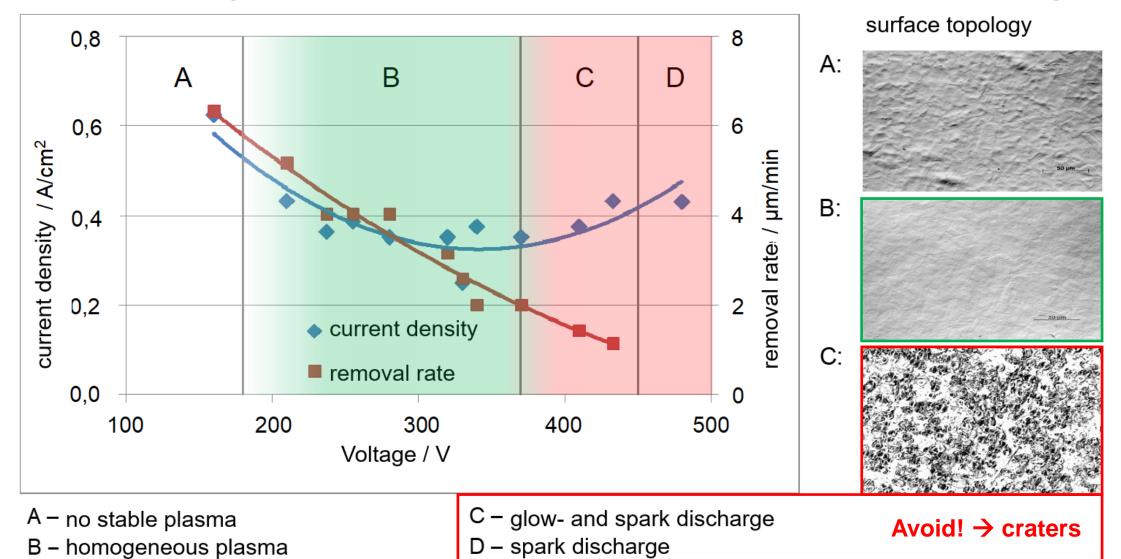
inside electro-hydrodynamic zone: VGE leads to high thermal isolation (\rightarrow T_{workpiece} = ~100 °C) and electrical isolation (high voltage drop \rightarrow ionisation / plasma)



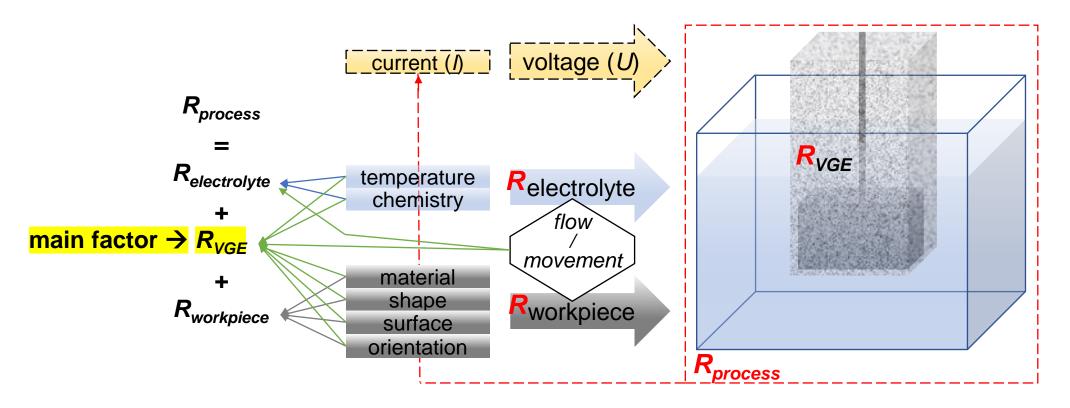
voltage limit shifted up or down, depending on resistance of system



upper voltage limit



electrical resistance and current



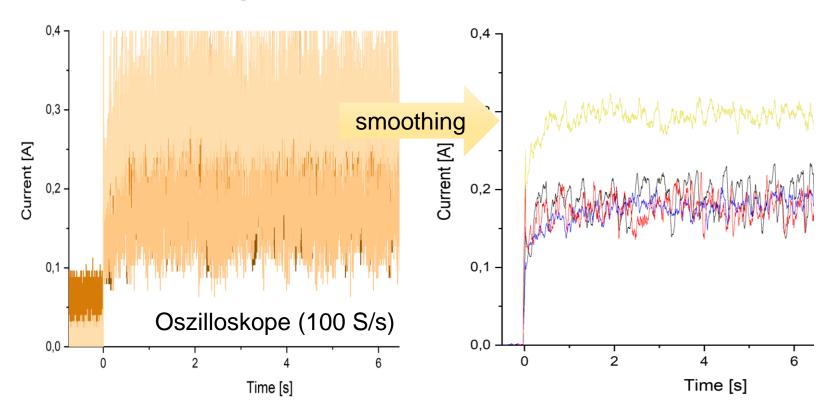
 \rightarrow Ohm's law: $I = U/R_{process}$

the resulting current(flow) is the main driver of the PeP-process (and also the main live-value/parameter to characterise the process)

 \rightarrow Amount of charge $Q(t) = \int I(t)dt$ most important/correct parameter on the input-side to describe "how much PeP" was done



measurement current/charge



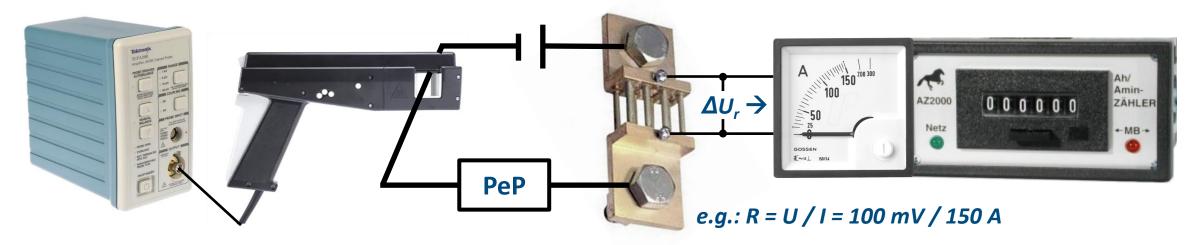


PeP is a highly dynamic process: 10³ to 10^x? current jumps/second with large amplitudes

- → most exact measurement by oszilloskop, but: hard to read and lot of data → need of smoothing
- → digital displays: live values not good to read (fast changing)
- → physical needle analog meter (slugish behaviour = smoothing): good and simple to read



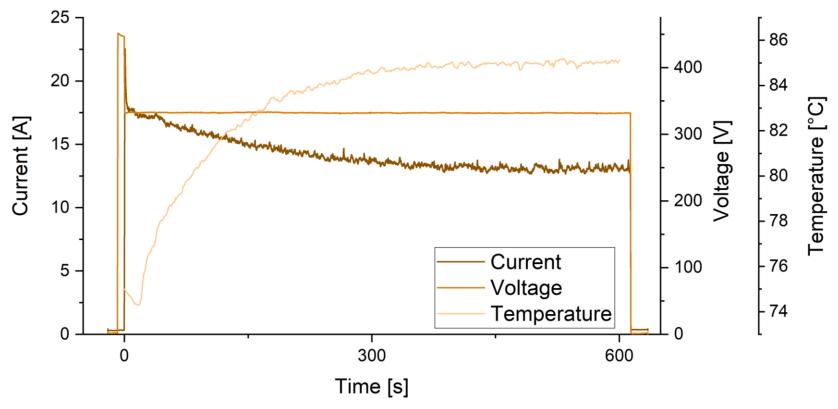
measurement of current/ charge



	current probe + amplifier	shunt	charge integrator
principle	magnetic field of cable + Hall effect	voltage drop of a defined resistor (I = U / R)	voltage drop of shunt → integrating current over time
advantages	current circuit not affected contactless easy to use and safe	high accuracy (also current spikes) direct measurement cost-effective	easy to read cost-effective
dis- advantages	less accuracy at low current sensitiv to magnetic fields over range spices problematic expensive	circuit interuption → (small) voltage drop	



current and temperatur



- current spike due to fast immersion of the part and formation of VGE
- continuos drop of current due to increasing temperature and smoothing of surface and so decreasing the real surface area



current and temperatur

I = U / R and U is constant

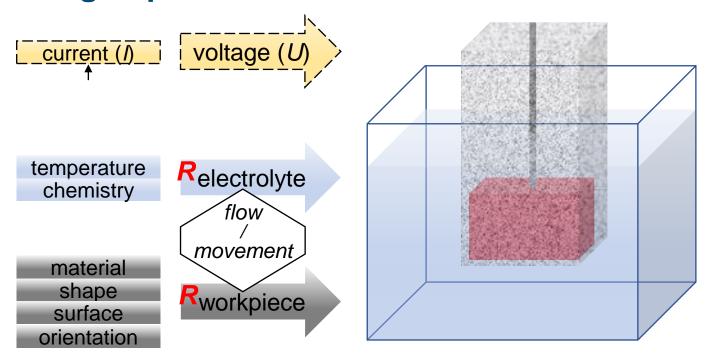
- → when measured current is lower at higher tempertures then the (total) resistance must be higher
- higher temperatur of workpiece: → higher resistance
- higher temperature of electrolyte: → higher mobility of ions → lower resistance but
 - → thicker VGE (?) → higher resistance

I = U / R and U is increased

- → current should be higher but there is no clear effect to see (compare to slide: upper voltage limit)
- higher voltage can influence chemical, physical and plasma processes so that the recistance is also increased and in total the current not increases



current density

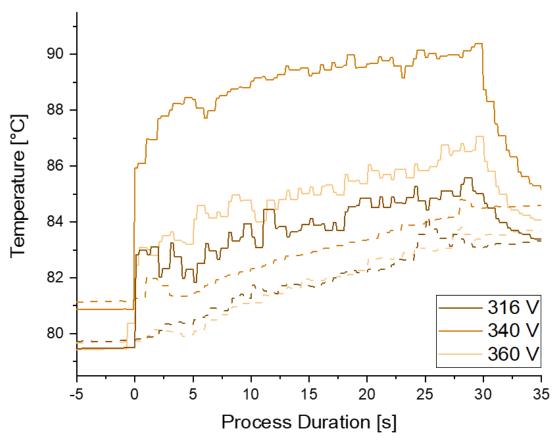


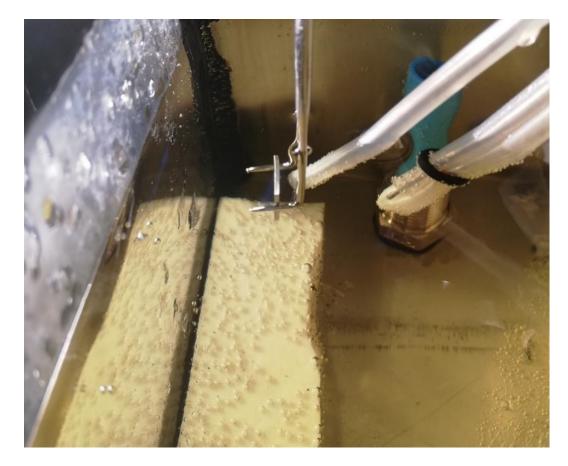
 $\vec{J} = I/A_{workpiece}$...typically given in A/cm^2 is a value, that can describe how intensive the process works on the part

- → mainly affected by the conductivity (chemistry + temperature) of electrolyt and workpiece
- → typicall values: 0.1 0.4 A/cm²



temperature



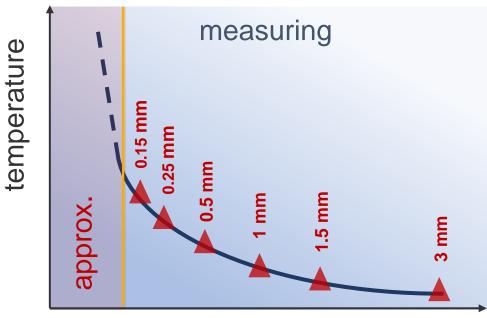


- electrolyte has not "one temperature", it depends where it is measured

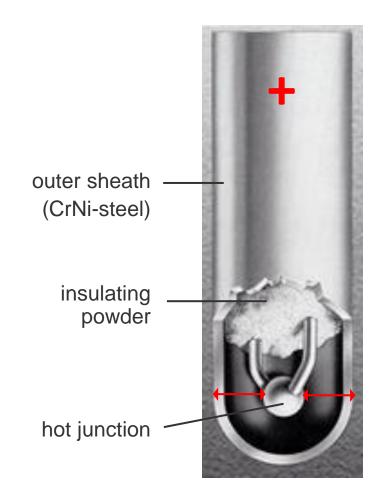


temperature

What's the temperature of plasma?
Can we measure it with thermocouple?

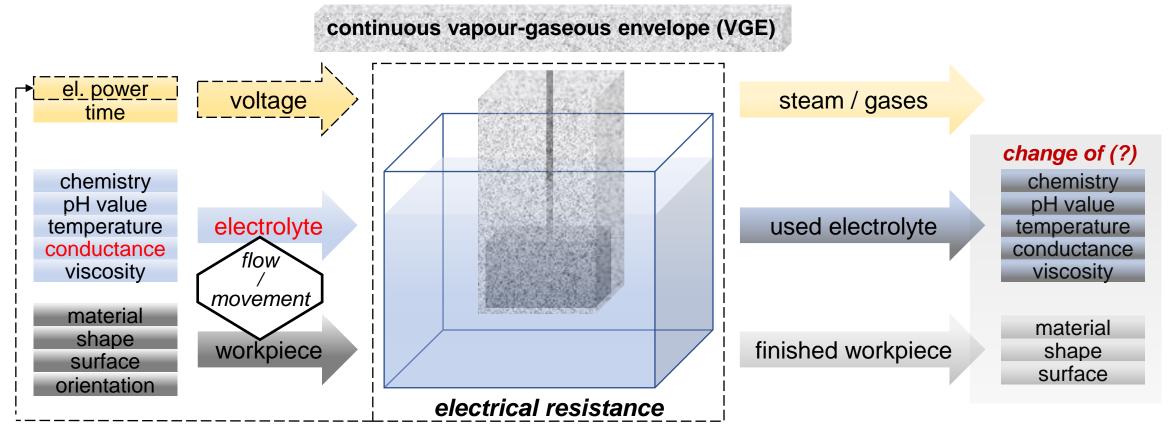


distance plasma – hot junction





conductance of electrolyte solution



- conductivity (κ) of electrolyte mainly influenced by the amount of solved salts/additives and it's temperature
- influences total resistance (R) and thickness/stability of VGE: → higher κ → lower R of electrolyte and thinner VGE (also lower R) → higher current → can increase material removal, but also surface roughening



conductance



- conductivity meter with measurement cell with 2 or 4 electrodes
- AC voltage applied across electrodes → depending on resistant between electrodes a measuring current flows
- measured resistance is converted into conductivity in mS/cm (typical unit for PeP) by: $\kappa = K/R$
- with the cell constant K = d/A, influenced by distance (d) and area (A) of the electrodes

our target: conductance κ of 100 – 140 mS/cm @ starting temperature (mostly 75 – 80 °C)



material removal rate

material removal rate (MRR):

- mainly used to describe how fast PeP works (e.g. given in gramm per minute)
- influenced by a lot of factors:
 - part (material, geometry, size, surface (+area) and it's orientation (and or it's movement)
 - electrolyte (conductance, chemical reaktions, temperature, lifetime) and it's flow
 - process: voltage → current/amount of charge (time)
- → very specific value and difficult to compare if more than one condition is changed (and most are changing even during the process itself!)

sometimes better to find other specific rates:

- material removal per charge (gramm per ampere minute)
- material removal per area (gramm per cm²)
- change of dimensions per time (µm/min) / per charge (µm/Amin) / ...



observations from the praxis

higher temperature: lower MRR but higher material removel per charge

→ PeP is slower but more efficient

higher temperature: higher removal at spikes (burrs, edges,...) than on flat areas



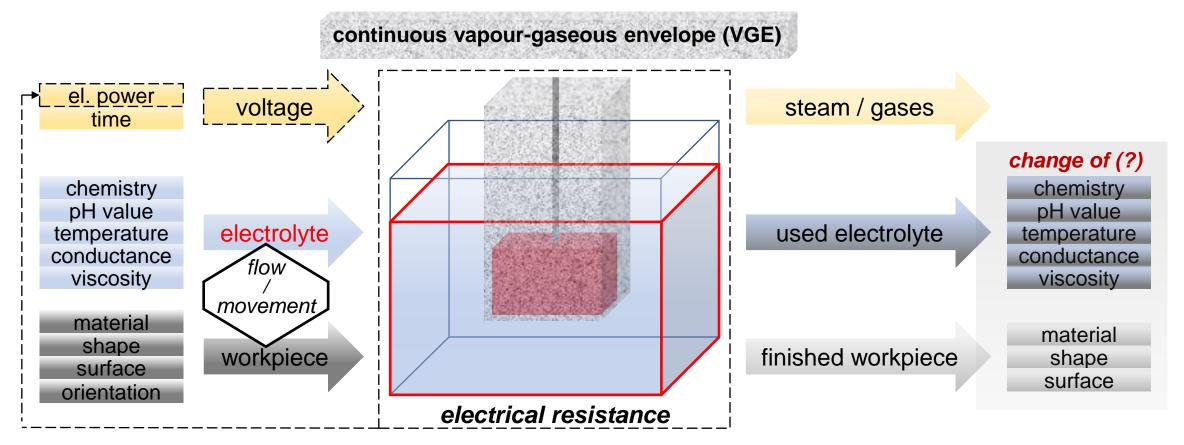




UNDERSTANDING PEP

Part 2: Electrolyte Solutions

electrochemical cell

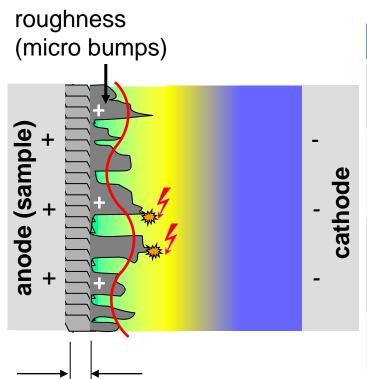


- chemistry of electrolyte solution is really important to achive material removal, surface smoothing and gloss
- → well working electrolyte composition has to be found for each single material/alloy



Material Removal Mechanisms

combination of electrochemical and physical processes

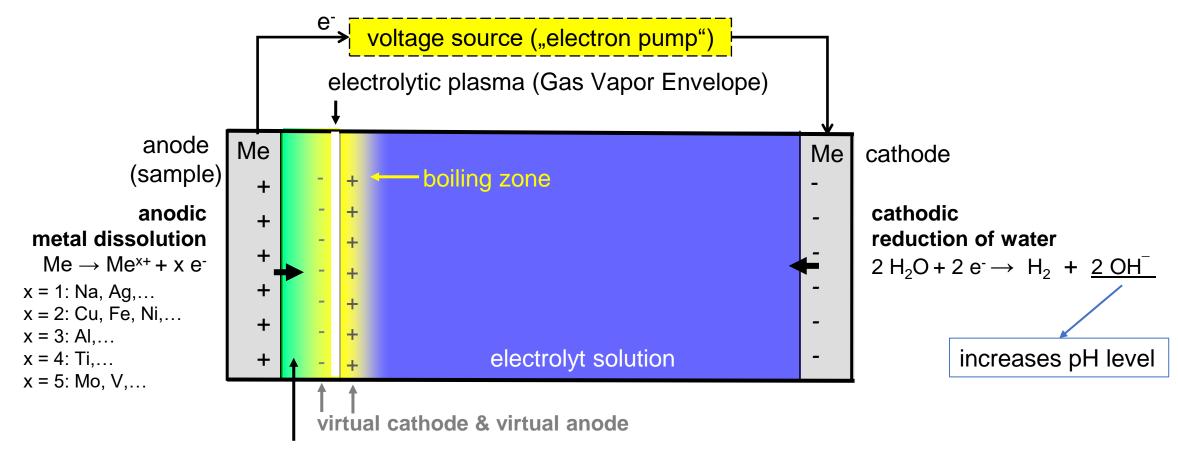


mechanism	
electrolytic dissolution	applied voltage → electric field forms → metal ions dissolve from surface into electrolyte
plasma discharge	high voltage → plasma region with high-energy ions, electrons, and neutral atoms (highly reactive) → enables material removal from surface by preferentially attacking microscopic peaks
oxidation + chemical reactions	plasma state and presence of oxygen → forming of less stable oxides on surface → easier to remove
gas evolution	gas bubbles + rising → remove of abraded material residues

Processing boundary layer (energetically activated area)



electrochemical cell/ reaction zones



highly concentrated layer around the anode (Helmholtz, Gouy-Chapman)

boiling point 104 -108 °C (= max. temperature of anode, discussed differently in literature)



reaction zones/electrochemical cell

Possible anode reactions under the conditions of PEP [80].

	Reactions	Potential (V) vs SHE	Reaction #
initial reactions at anode / cathode	$Cr + 2H_2O \rightarrow Cr(OH)_2 + 2H^+ + 2e^-$	-1.1	(7)
	$Cr(OH)_2 + H_2O \rightarrow Cr(OH)_3 + H^+ + e^-$	-0.6	(8)
	$Fe + H_2O \rightarrow FeOH^+ + H^+ + 2e^-$	-0.4	(9)
Further reactions with water and/or other ions in electrolyte	FeOH ⁺ + H ₂ O \rightarrow Fe(OH) ₂ ⁺ + H ⁺ + e ⁻	0.3	(10)
	Cr(OH) ₃ + H ₂ O \rightarrow CrO ₄ ²⁻ + 5H ⁺ + 3e ⁻	0.4	(11)
	Fe(OH) ₂ ⁺ + 2H ₂ O \rightarrow FeO ₄ ²⁻ + 6H ⁺ + 3e ⁻	0.7	(12)
	2H ₂ O \rightarrow 4H ⁺ + O ₂ + 4e ⁻	0.8	(13)
	2H ₂ O \rightarrow H ₂ O ₂ + 2H ⁺ + 2e ⁻	1.8	(14)
	2SO ₄ ²⁻ \rightarrow S ₂ O ₈ ²⁻ + 2e ⁻	2.0	(15)





role of electrolyte

main task: absorption + retention of metal ions in solution

- water: → oxidation of Me
 - → "produce" VGE
- salts: → deliver ions as "charge carriers" (mainly responsible for conductance)
- additives: eg. acids, bases, complexing agents
 - → in some cases: remove oxid layer (anodic) to start the process
 - → keep anodic reaction products in solution (e.g. metal ions or oxides)
 - > prohibit formation of metal oxides on the metal surface

Electrolyte solution needs to deliver a suitable medium (environment, e.g. pH-level) to enable material removal, surface smoothing and increase of gloss!



examples

CrNi-steel @ acidic ammonium sulfate solution (sulfuric acid)

	Fe	Cr	Ni
Initial reaction (at anode)	Fe → Fe+ 2e-	$Cr \rightarrow Cr^{3+} + 3e^{-}$	Ni → Ni ²⁺ + 2e ⁻
Further reaction	$FeOH^+ + H_2O \rightarrow Fe(OH)_2 + e^- \dots$	$Cr^{3+} + SO_4^{2-} / NH_4^+ \rightarrow$	Ni ²⁺ + SO ₄ ²⁻ →
Further reaction products	\rightarrow (NH ₄)Fe(SO ₄) ₂ \rightarrow Fe(OH) ₃	\rightarrow $Cr_2(SO_4)_3$ \rightarrow $(NH_4)Cr(SO_4)_2$	→ NiSO ₄
Soluble (pH value)	< ~ 3	< ~ 5 and > ~ 9	> ~ 10
if not: precipitation of	insoluble red-brown depositions + mud	olive-green CrO(OH)- particles	light-green Ni(OH) ₂ -particles

- pH < ~1.8: chemical etching (also without voltage) → rought and matte surface!
- content of Fe > ~72 % → firmly adhering black oxid-layer (FeO and/or Fe₃O₄)



examples

CrNi-steel @ sodium carbonate solution

	Fe	Cr	Ni
Initial reaction (at anode)	nearly no reaction of Fe	$Cr \rightarrow Cr^{3+} + 3e^{-}$	Ni → Ni ²⁺ + 2e ⁻
Further reaction	because oxidation of O ₂ is energetically more favorable	$Cr^{3+} + OH^{-} \rightarrow Cr(OH)_{3}$	$Ni^{2+} + CO_3^{2-} \rightarrow NiCO_3$
Further reaction products	$(2 \text{ Oh}^{-} - 4e^{-} \rightarrow \text{ O}_{2} + \text{H}_{2}\text{O})$	$CrO_4^{2-}/$ $2 Na^+ + CrO_4^{2-} \rightarrow Na_2CrO_4$	
Soluble (pH value)		> ~ 9	good
if not: precipitation of		yellow sediment	light green

very very low material removal when polishing CrNi-steel in sodium carbonate solution but high gloss

Caution!: Fe-rich surface → lower oxidation resistance



CrNi-steel @ sodium carbonate solution

typical: orange glowing of ionised sodium



examples



examples

Copper @ acidic ammonium sulfate solution

→ development of copper sulfate layer (CuSO₄) on anode

Copper @ ammoniacal ammonium sulfate solution

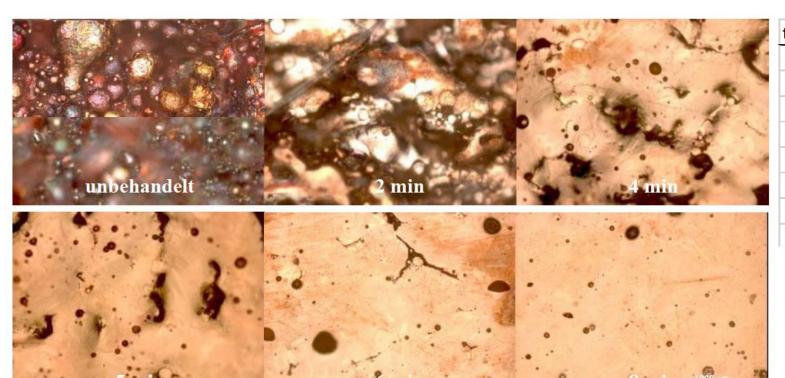
	Cu			
Initial reaction (at anode)	Cu→Cu ²⁺ + 2e ⁻			
Further reaction	$Cu^{2+} + 4NH_3 \rightarrow [Cu(NH_3)_4]^{2+}$	$Cu^{2+} + 2OH^- \rightarrow Cu(OH)_2$		
Further reaction products	$[Cu(NH_3)_4]^{2+} + 2OH^- \rightarrow Cu(OH)_2 + 4NH_3$	CuO·H ₂ O		
рH	8.1 – 8.7	< ~ 9		
if not: precipitation of	CuSO ₄	unsoluble particles on anode		

- ammonia (NH₃) acts as complexing agent and stable [Cu(NH₃)₄]²⁺ is formed (Only between pH 8.1 8.7 and NH₃ is present! If not: light blue depositons and/or no gloss)
- high material removal rates + good surface smoothing + high gloss achievable



examples

e.g.: Copper @ ammoniacal ammonium sulfate solution works well (see e.g. roughtness)



t [min]	Ra	Rq	Rz
0	11,15		73,85
2	3,30	3,60	13,71
3	1,96	2,51	8,45
4	1,40	1,83	7,35
5	1,01	1,31	5,71
6	0,56	0,88	4,65
7	0,49	0,71	2,89
8	0,44	0,71	3,48



difficult materials and options

material	difficulties	options
low-alloy steel	rust and chemical etching	no strong acids → use citric acid
carbon-rich steel	graphit-coating of cathode	?
valve metals/alloys (Al, Ti, Zr)	hard-to-destroy oxide layers, matte surfaces	fluoric acid (!)
Si-rich alloys	matte grey surfaces, no gloss	?



post-treatment

- normaly its enough to rinse with water
- high gloss surfaces tend to show water spots → deionised water and fast drying with pressurised air
- corrosion sensitive metals/alloy: well washing + rinse with ethanol + drying (oven), store dry and in protective atmosphere, (i.e. oil-bags or in ethanol), don't touch with bare hands
- rust from already corroded materials can be removed by PEP-treating them in citric acid-based electrolyte



preparation of electrolyte solution

target: conductance κ of 100 – 140 mS/cm @ starting temperature (mostly 75 – 80 °C)

⇒ salts (e.g. ammonium sulfate, ammonium chloride, sodium carbonate) = basic for conductance approximation: aqueous solutions ⇒ increase of conductivity = $\sim 2 - 3$ % per K (range between 25 – 100 °C) conductance κ depends on concentration c and molar conductance λ of ions (Xⁿ⁺ and Xⁿ⁻):

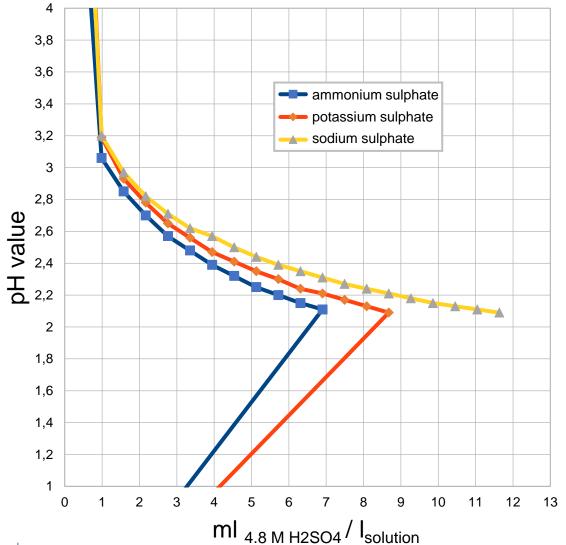
$$\kappa = \mathbf{c} \cdot (\lambda_{Xn+} \cdot [X^{n+}] + \lambda_{Xn-} \cdot [X^{n-}])$$

target: suitable medium/environment (pH value) for required chemical reactions with anodic material

→ use of: acids, bases, complexing agents,...

other additives may influence conductance \rightarrow take into account using the equation above!





preparation of electrolyte solution

charts for resulting pH values (measurements) for different sulphatic solutions dependig on added 4.8 M sulphuric acid (ml/l)

→ easy to read and practical and for daily work



preparation of electrolyte solution

The regimes of steels PEP and the results obtained. Some data are rounded, in some cases, average values are indicated instead of the declared intervals.

Composition of aqueous solution (wt%)	Samples material	U(V)	T_{el} (°C)	t (min)	Ra (µm)	Ref.
4% ammonium sulphate and 0.25% hydrochloric acid	12Cr18Ni10Ti	270	35-40	5	0.02(0.20)	[109]
5% ammonium sulphate	20Cr13	250	70	15	0.06(0.45)	[55]
Sulphates of ammonia and sodium up to 30 g/l	AISI 201	250			0.06(0.24)	[61]
2% ammonium chloride	Low-carbon steel	300	85	15	0.09(0.63)	[106]
6% ammonium sulphate	20Cr13	300		15	0.13(0.53)	[106]
0.2 mol/l sodium sulphate	15CrMoV	320		10	0.14(0.39)	[111]
4% ammonium sulphate and 1% disodium ethylene diamine tetra acetate (Trilon B)	03Cr16Ni15Mo3	330	85-90		1.40(5.60)	[112]
0.24 mol/l ammonium chloride	30CrMnSi	311	_	8	0.17(0.93)	[107]
4-6% neutral salts	CrNi 18/10	_	65	5	0.78(1.70)	[59]
5% ammonium sulphate	20Cr13	300	70	15	0.06(0.32)	[99]
4% ammonium sulphate and 0.2% hydrochloric acid	08Cr18Ni10Ti	_	35-40	6	0.08(0.42)	[58]
0.2 mol/l ammonium sulphate	12Cr18Ni10Ti	380	85-90	3	0.65(1.80)	[126]
3% ammonium chloride and 1% ammonium sulphate, 0.5% Trilon B	38Cr2Ni2Mo	270	90	5	0.40(1.60)	[66]
8% ammonium sulphate	CrNi45MoWTiAlNbB	300	80	-	0.15(0.80)	[84]
5% ammonium sulphate	08Cr18Ni10Ti	270	85-90	5	0.17(0.63)	[117]
3% ammonium sulphate	SUS304	280	17	35	0.06(0.40)	[118]
18% sodium hydrocarbonate	12Cr18Ni10Ti	260	85		0.06(0.64)	[67]
5% ammonium sulphate and 0.8% Trilon B	CrNi45MoWTiAlNbB	300	73	2	0.18(0.60)	[120]
5-7% ammonium sulphate	12Cr18Ni10Ti	295	85-90	8	0.16(0.63)	[122]
3.4% ammonium sulphate	20Cr13	300	50-65	_	0.02(0.12)	[149]

ammonium sulphate is often used because it (nearly) not take place in reaktions → no loss of it



preparation of electrolyte solution

Calculation for amount of acid to be added to water / pH value example of a acidic 0.33 M ammonium sulfate solution (sulphuric acid)

Henderson-Hasselbalch equation: $pH = pK_a + log(c(A^-) / c(HA))$

```
pH... acidity of the solution
```

p K_a ... negative base-10 logarithm of the acid dissociation constant K_a (acid dissociation constant at equilibrium state) (1.99 for H_2SO_4 at equilibrium of hydrogen sulfat/sulfat)

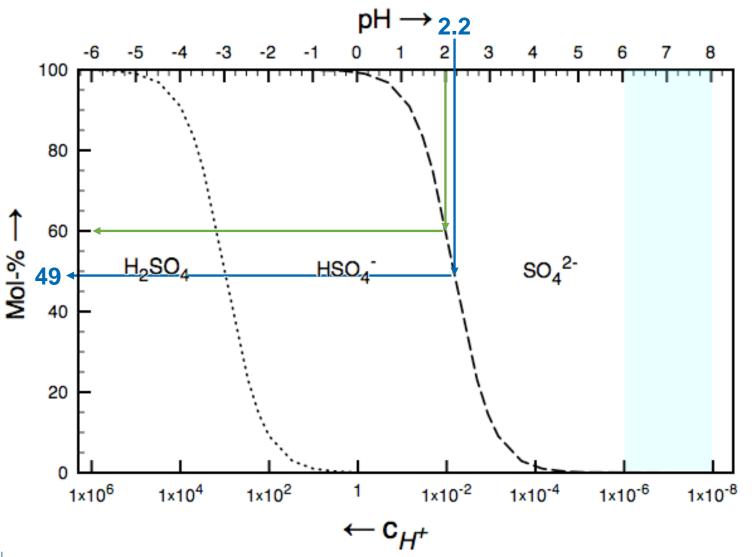
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c(A^{-})... concentration of the conjugate base / negative ion (SO_4^{2-})
```

c(HA)... concentration of the associated acid (HSO_4)

```
⇒ c(HA) = c(A^-) / 10^{pH - pKa} 0.33 \text{ mol/l} / 10^{2.2 - 1.92} = 0,1732 \text{ mol/l} ??? → pH 2,71 ???
⇒ c(HA) = c(A^-) / 10^{pH - pKa} = 0.33 \text{ mol/l} / 10^{2.2 - 1.99} = 0,2035 \text{ mol/l} ??? → pH 2,2 ???
```



preparation of electrolyte solution



pH 2.2 → 49 Mol-% HSO₄ equilibrium to 51 Mol-% SO₄²⁻

pH 2.0 → 60 Mol-% HSO_4^- equilibrium to 40 Mol-% SO_4^{2-}



preparation of electrolyte solution

Example: acidic 0.33 M ammonium sulfate solution (pH ~ 2.2)

- Calculation of incredient ammonium sulfate (44 g/l)
- Mixing (increased temperatur ~50 °C)
- pH (water + 0.33 M ammonium sulfate) $\sim 6.3 6.4$
- Calculation of incredient sulfuric acif (ca. 5.5 ml 4.8 M sulphuric acid / l)
- Slow dosing of sulfuric acid
- (Calculation of conductance)



lifetime of electrolyte

lifetime:

- counted in the amount of charge as a value for how much metal is solved in electrolyte
- ends when required needs could not be achieved any more (gloss/roughtness or low MMR)
- mostly first gloss requirements could not be achieved but material removel is still given refreshing:
- bring out metal elements by taking him the ability to solve them, e.g. change it's pH value → different metal compounds precipitate from the solution
- flocculating agent are helpfull to increase the agglomeration of small partikels
- sedimentation + decantig or filtering
- add required substances to bring it back to ist initial state (pH value)



environmental and user safety

Safety issue	Precaution		
Hydrogen gas formation on the cathode	Gas exhaustion system		
Hot electrolyte	Heat resistant work cloths		
Chemical hazard	Safety glasses, gloves, lab coat, other equipment		
Direct voltage	Electrical insulation		
Halides are oxidised during PEP	Filtration system built-in in the gas exhaust system		
Consumed electrolyte	Should be disposed according to the environmental safety requirements, i.e. cannot enter wastewater system		



Werkstück-Prozessträgersystem energiequelle (DC) Elektrolyt Kathodenkontakt (Elektrolytbad) Verdampfter Elektrolyt (Blasen und Anodenkontakt Dampfschicht) (Werkstück) Werkstück Plasmazone Elektrolyt-einheit (Temperatur-Becken regelung) Kathode Elektrolytzulauf Elektrolytrücklauf

environmental and user safety







